

A wide-angle photograph of the Grande Dixence Dam, a massive concrete gravity dam. The dam is situated in a deep, rocky gorge. Water is seen cascading down the face of the dam in numerous small, white, frothy streams. The sky above is a clear, pale blue. The surrounding cliffs are dark and rugged, with some sparse green vegetation. The overall scene conveys the immense scale and power of the structure.

EPFL Heightening of very high gravity dams

The case study of the Grande Dixence Dam

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Introduction

Context:

- Energy Transition in Switzerland
- Mitigation of the effects of climate change

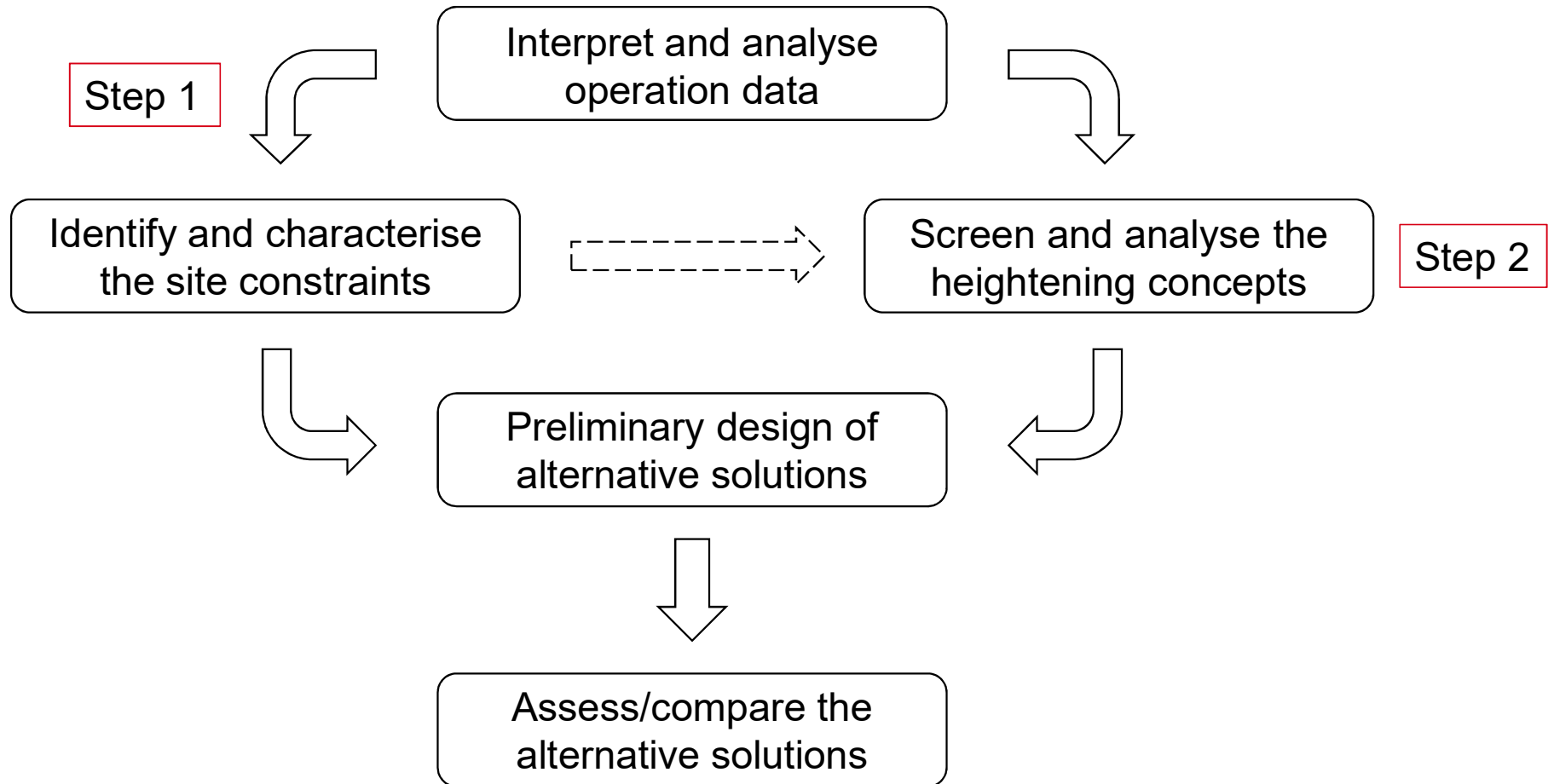
Motivation:

- Large incremental positive impacts on storage with low negative impacts
- Very high gravity dams are well studied and documented
 - Availability of monitoring data and safety assessment tools

Objective:

- Establishment of a general approach to identify and develop solutions for the heightening of very high gravity dams
 - Application to the case study of the Grande Dixence Dam

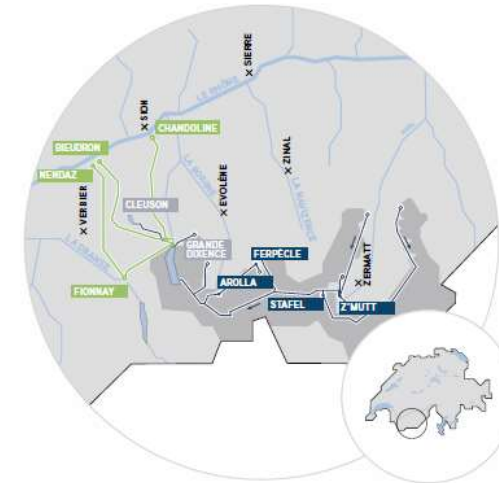
Methods



Case study: The Grande Dixence Dam

The scheme

- 420 km² watershed
- 100 km of galleries
- 5 pumping stations
- 3 power plants

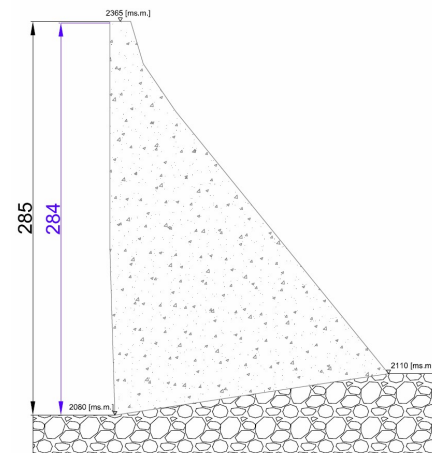


Grande Dixence scheme

The dam

- World highest gravity dam
- Creates a reservoir of 400 hm³

Characteristics	
Height	285 m
Base width	200 m
Dam crest width	15 m
Dam crest developed length	700 m



Dam central cross-section



Dam's downstream view



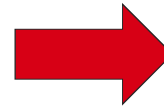
Dam's crest

Open theme | Basile Clerc | Milano, 09.09.19

Results: Additional water supply and available storage

- Actual water supply and future estimations

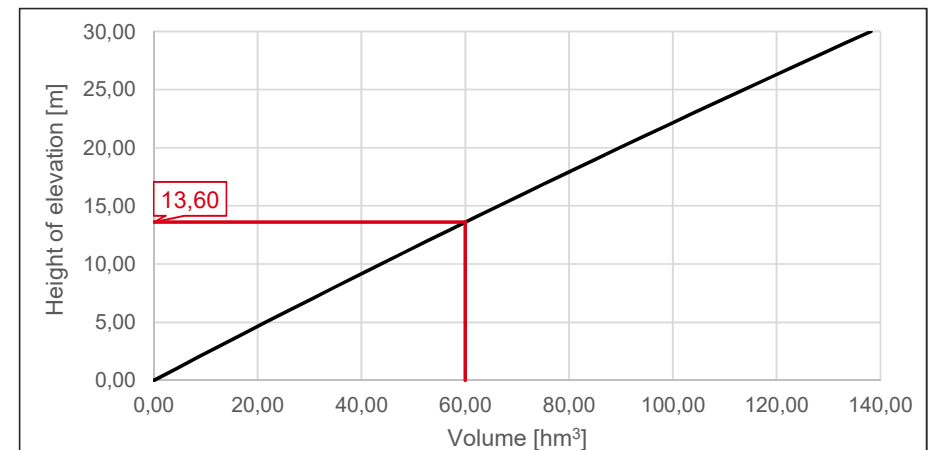
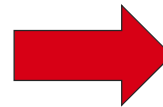
Year	Accumulated volume [hm ³]
2011	504
2012	540
2013	481
2014	451
2015	548
2016	478
2017	525
Average	504



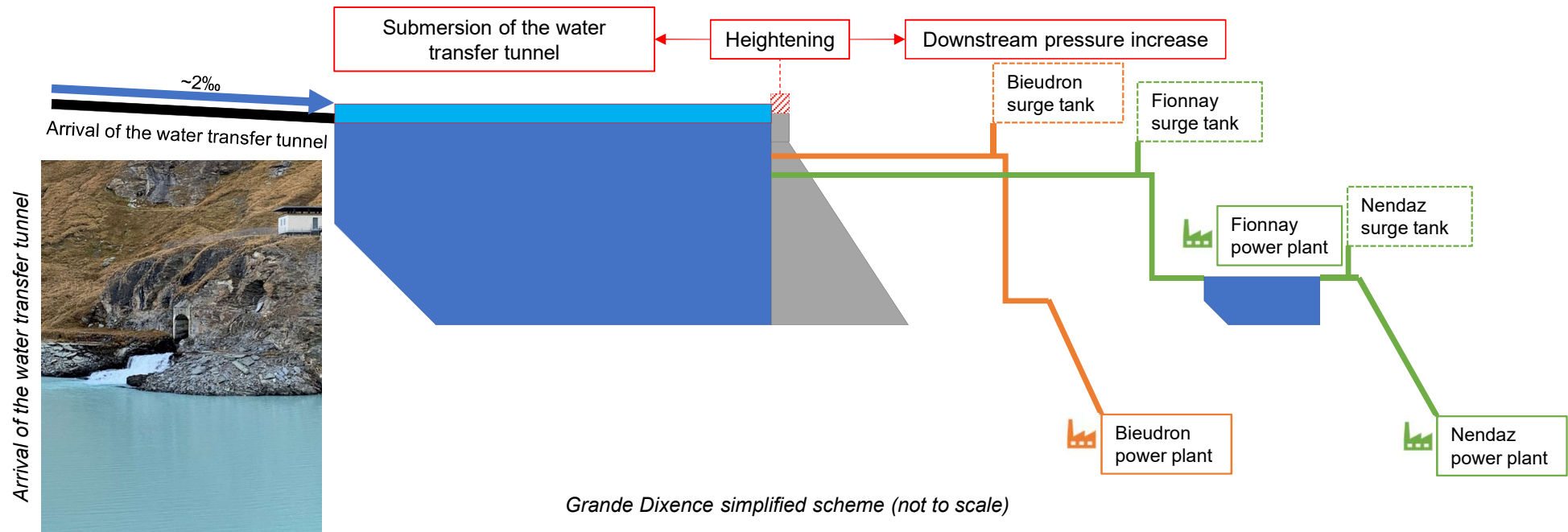
- Average additional volume of 100 hm³
- Future estimations show a water supply decrease

- Indicative additional volume and corresponding height

- Smaller indicative additional volume of 60 hm³
- More viable and profitable on the long-term



Results: Site constraints



Submersion of the water transfer tunnel

- Backwater effects modifying pumping
- Aerations issues farther upstream

Downstream pressure increase

- Impact on downstream surge tanks
- Fionnay surge tank requires adaptation measures

Results: Screening of heightening concepts

Several heightening solutions were considered:

- Gravity dam
- Arch dam
- Multiple-arch dam
 - Use of post-stressed anchors
 - Build artificial abutments

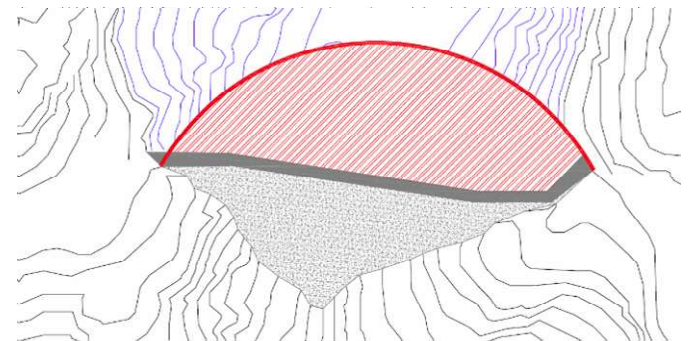
Constraints:

- Valley and dam shape
- Dam joints every 16 m
- Dam height
- Prohibitive conflicts with hydropower must-run operation

➤ Gravity dam heightening was retained for preliminary design



Top view of Grande Dixence dam

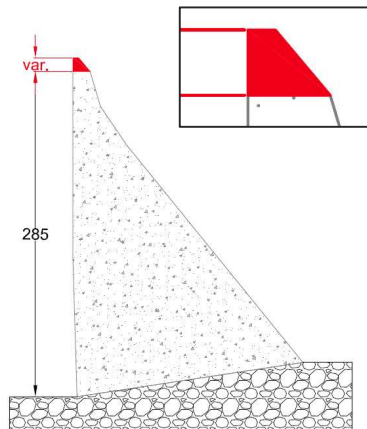


Implementations of dam heightening

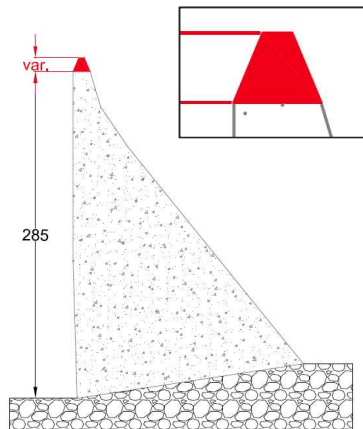
Results: Heightening options

New crest width of 5 m for all solutions

Variant 1
«Standard»

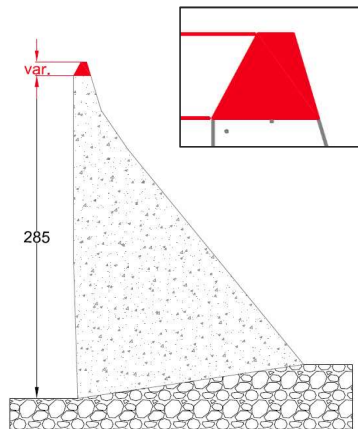


Variant 2
«Symmetrical»



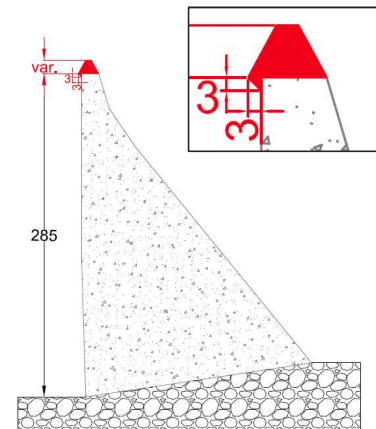
- Favourable hydrostatic pressure
- Better weight balance

Variant 3
«Asymmetrical»



- Increased favourable hydrostatic pressure
- Heightening weight farther downstream

Variant 4
«Offset»



- Favourable hydrostatic pressure
- Creation of a cantilever
- Greater load upstream

Results: Stability and structural analysis

Verifications:

- Sliding stability
- Overturning stability
- Ultimate resistance

Verified elevation heights:

- 6, 9, 12 and 15 m

All calculations were made considering a normal load case and a full lake.

Using two models:

- Analytical
- Computational

Design criteria:

- Based on the recommendations of “Directive on the Safety of Water Retaining Facilities” established by Swiss Federal Office of Energy
- Higher tensile resistance criterion of 1 MPa

Results: Analytical model

■ Sliding stability

$$S_G = \frac{\left[\frac{(tg\varphi \sum N)}{\gamma_{m\varphi}} \right] + \left[\frac{(cA)}{\gamma_{mc}} \right]}{\sum T} \geq 1.0$$

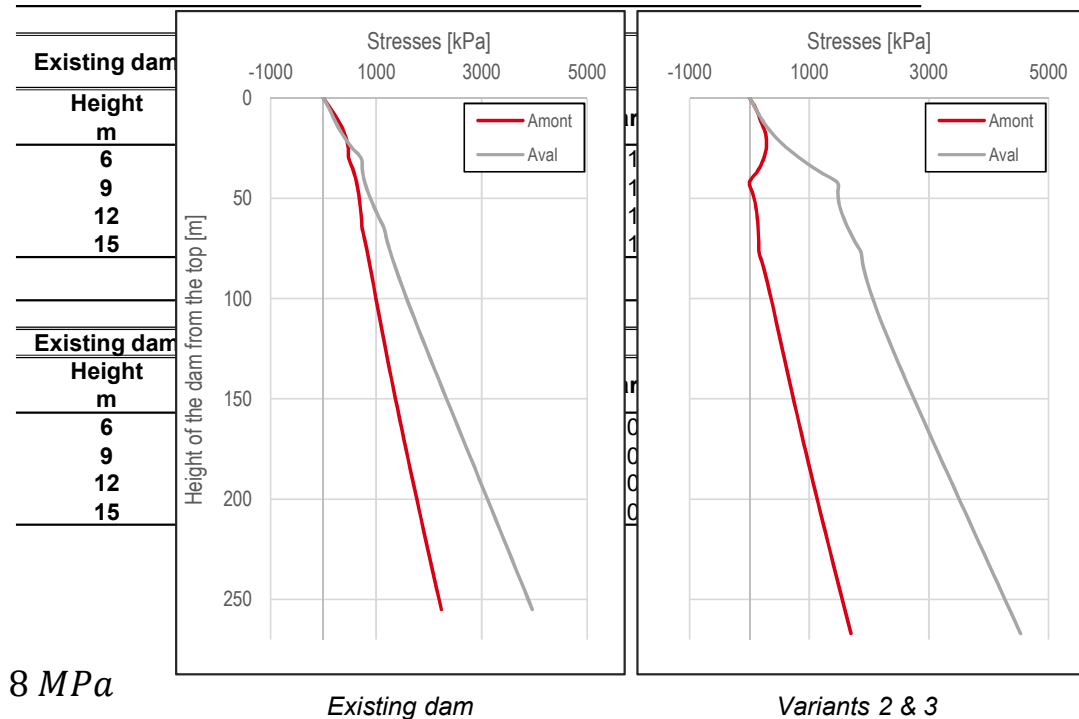
■ Overturning stability

$$0.33 < X = \frac{R_x}{B_B} < 0.66$$

■ Ultimate resistance

$$-1 \text{ MPa} \leq \sigma_{z,up} = \frac{6}{b^2} \left[G \left(\frac{2}{3}b - x_G \right) - W \frac{z_W}{3} \right] \leq 8 \text{ MPa}$$

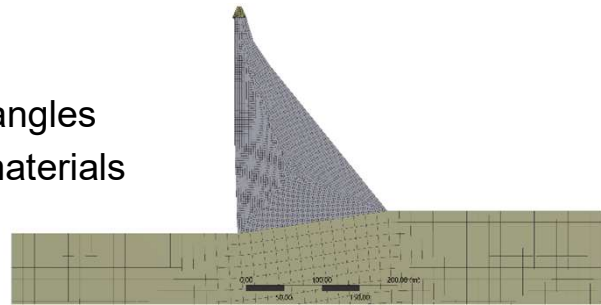
$$-1 \text{ MPa} \leq \sigma_{z,dw} = \frac{6}{b^2} \left[G \left(x_G - \frac{b}{3} \right) + W \frac{z_W}{3} \right] \leq 8 \text{ MPa}$$



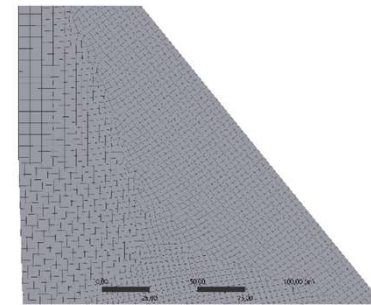
Results: Computational model

- Using *ANSYS Workbench* (2017) in 2D

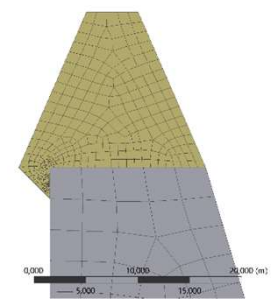
- Three main elements
- Different mesh size
- Quadrilaterals and triangles
- Standard values for materials
- Two friction surfaces



Foundation mesh: Elements of 15 m

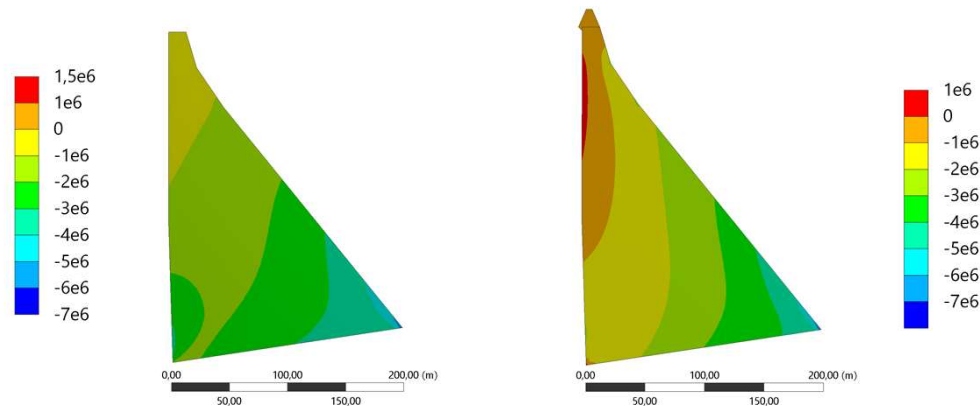


Existing dam mesh: Elements of 3 m



Heightening mesh: Elements of 1 m

- Ultimate resistance



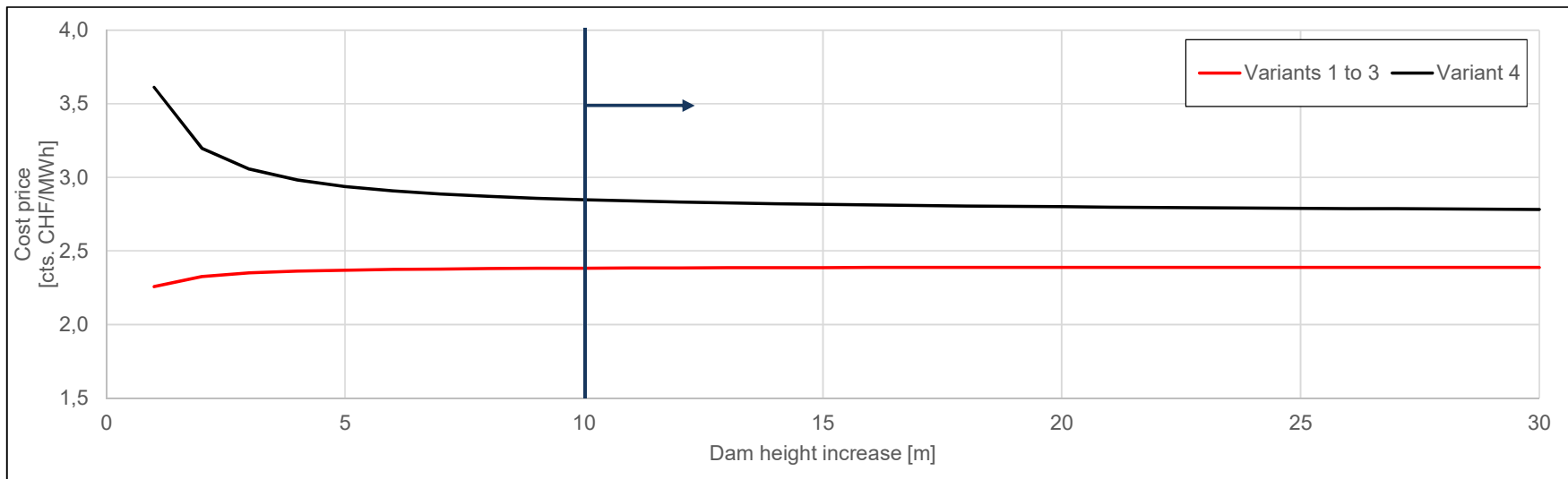
Normal stresses of existing (left) and variant 4, 15 m (right)

Results: Economic analysis

■ Levelized Cost of Electricity (LCOE)

Height of elevation m	Cost price cts. CHF/MWh	
	Variants 1 to 3	Variant 4
1	2.2578	3.6124
5	2.3691	2.9377
10	2.3827	2.8474
15	2.3866	2.8162
20	2.3879	2.7999
25	2.3883	2.7896

Little variation from 10 m



Conclusion

Establishment of a general approach ✓

Application to the case study of the Grande Dixence dam

- Determination of major constraints ✓
- Selection of a single heightening concept ✓
- Generation of four variants ✓
- Study of the overall behaviour of the heightened dam with two different models ✓
 - Satisfactory results for all variants
- Preliminary economic analysis ✓
 - Extremely low LCOE in comparison with other potential hydropower projects
 - **Height increase within 10 to 15 m is likely optimal**

Further investigations

- Adaptation of the water transfer tunnel, pressurized waterways and surge tanks



Thank you for your attention!