



**ICOLD**  
**INTERNATIONAL**  
**COMMISSION ON**  
**LARGE DAMS**



# **15<sup>th</sup> INTERNATIONAL BENCHMARK WORKSHOP ON NUMERICAL ANALYSIS OF DAMS**

## **Theme A**

### **SEISMIC ANALYSIS OF PINE FLAT CONCRETE DAM**

**9 September 2019, Milan, Italy**

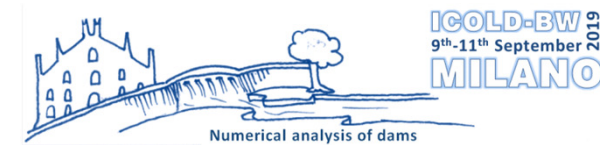
*Summary of the Benchmark Analysis Results*

*Study Cases D and F*

*Giorgia Faggiani - Ricerca sul Sistema Energetico - RSE S.p.A.*



## Case D and Case F: General info and requested results



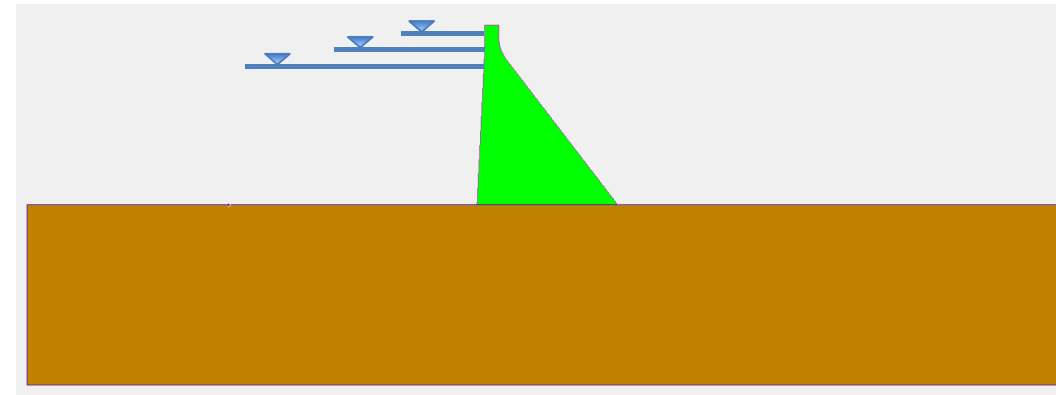
### Linear Dynamic Analysis for various reservoir levels

#### Case Studies

- **Case D:** foundation with mass & wave propagation approach
- **Case F:** massless approach

#### Required analyses

D-1	F-1	Winter Reservoir Water Level: WRWL	268.21 m a.s.l.
D-2	F-2	Summer Reservoir Water Level: SRWL	278.57 m a.s.l.
D-3	F-3	Normal Reservoir Water Level: NRWL	290.00 m a.s.l.



#### Input

- ☐ Geometry
- ☐ Material properties
- ☐ Static loads
- ☐ Seismic input (Taft)



**Given in  
formulation**

- ☐ FEM mesh
- ☐ FSI & SSI approach
- ☐ Boundary conditions

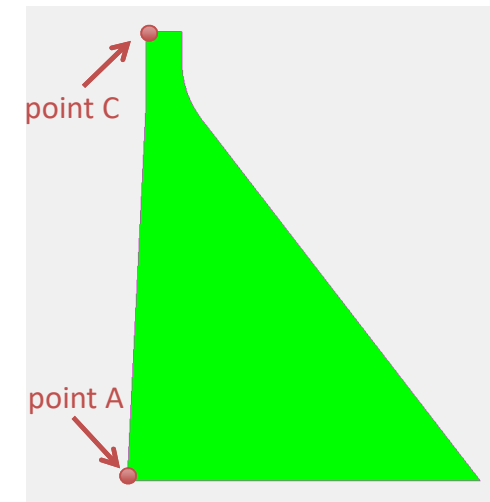


**Chosen by  
contributors**

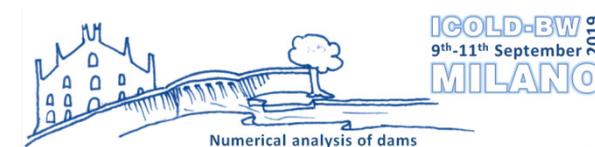
#### Output

- ☐ Hydrodynamic pressure TH at dam heel (point A)
- ☐ Total displacement TH at dam heel (point A) & crest (point C)
- ☐ Acceleration TH at dam heel (point A) & crest (point C)

**Only results for WRWL are here  
compared**



## Case D and Case F: Contributors choices



Contributor	FEM code	Integration scheme	Element size	Fluid-Structure Interaction	Fluid Type	Non-Reflecting BC	Free Field BC	Case D	Case F
11	Real ESSI	Implicit/explicit(FSI)	2 m	Acoustic-structural coupling	compressible	Domain reduction method to input motions with absorbing damping layers	No*	Y	
12	Diana	implicit	2.5-5 m	Acoustic-structural coupling	incompressible	lateral sides: 50m thick PML bottom: Free field BC	Only on the bottom*	Y	
13	Code_aster	implicit	10 m	Acoustic-structural coupling	compressible	Viscous-spring artificial boundaries	Yes	Y	
14	ANSYS	implicit	6 m	Acoustic-structural coupling	compressible	Infinite radiation boundaries	No	Y	Y
15	SAP2000	explicit	1 m	Links-gap	incompressible	Simple supports bottom: H & V restrictions lateral sides: V restriction	No	Y	
16	ABAQUS	implicit	3-6 m	Acoustic-structural coupling	compressible	Viscous-spring artificial boundaries	Yes	Y	Y
17	Parmac2D	explicit	3-5 m	Interface elements with only normal stiffness	compressible	Viscous boundaries (Lysmer and Kuhlemeyer)	Yes	Y	

Theme A - Pine Flat Dam

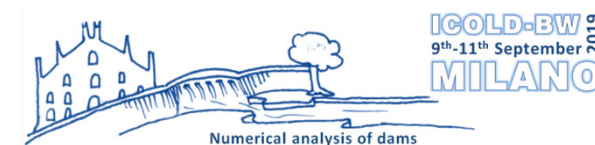
## Case D and Case F: Contributors choices



Contributor	FEM code	Integration scheme	Element size	Fluid-Structure Interaction	Fluid Type	Non-Reflecting BC	Free Field BC	Case D	Case F
18	Diana	implicit	3-30 m	Acoustic-structural coupling	compressible	Interface element with low stiffness and damping coefficient	No	Y	Y
19	Code_aster	implicit	15 m	Acoustic-structural coupling	compressible	Paraxial anechoic elements	Yes	Y	Y
20	ABAQUS	implicit	1.48 m	Acoustic-structural coupling	compressible	Viscous boundaries	Yes*	Y	
21	Code_aster	implicit	1-37.5 m	Acoustic-structural coupling	compressible	Absorbing BC (for fluid elements only)	No	Y	Y
22	Diana	implicit	2 m	Acoustic-structural coupling	incompressible	Viscous boundaries (variation of Lysmer and Kuhlemeyer)	Yes*	Y	Y
23	ANSYS	implicit	0.5-4 m	Acoustic-structural coupling	compressible	Viscous-spring artificial boundaries	No	Y	Y
24	FLAC-3D	explicit	7.2 m	Mixed discretization scheme	compressible	Viscous boundaries (Lysmer and Kuhlemeyer)	Yes	Y	Y
25	Diana	implicit	2.5-4 m	Fluid like structural elements	incompressible	Interface element (Lysmer and Kuhlemeyer)	Yes*	Y	

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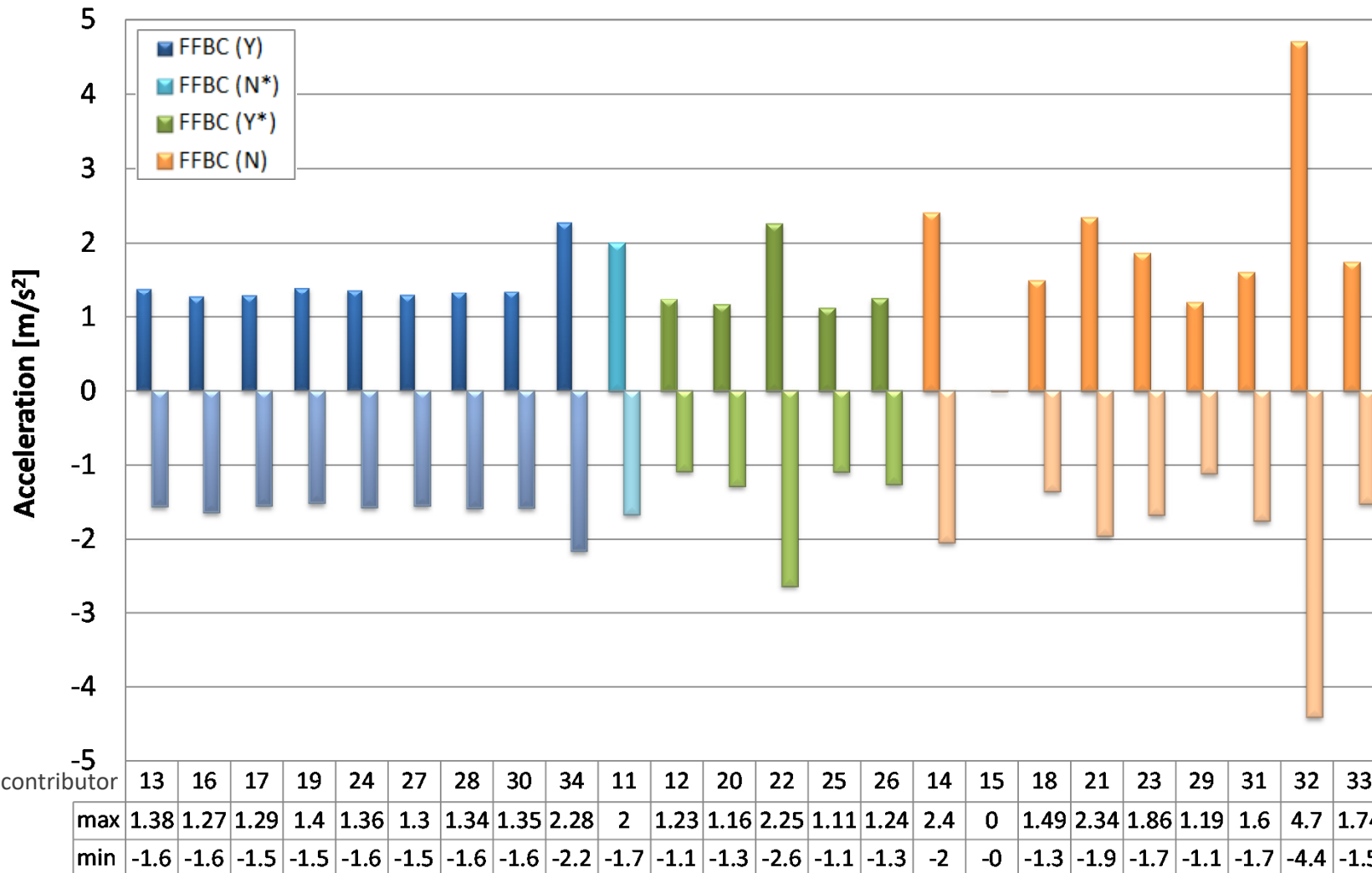
## Case D and Case F: Contributors choices



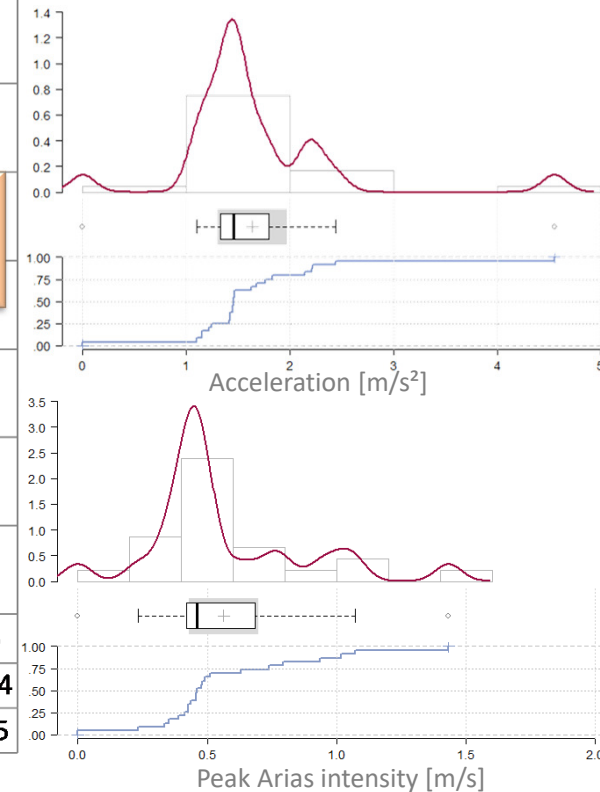
Contributor	FEM code	Integration scheme	Element size	Fluid-Structure Interaction	Fluid Type	Non-Reflecting BC	Free Field BC	Case D	Case F
26	ABAQUS	implicit	1 m	Acoustic-structural coupling	compressible	Infinite acoustic elements (Lysmer and Kuhlemeyer)	Yes*	Y	Y
27	Parmac2D	explicit	3-5 m	Interface elements with only normal stiffness	compressible	Viscous boundaries (Lysmer and Kuhlemeyer)	Yes	Y	
28	ABAQUS	implicit	1.5 m	Acoustic-structural coupling	compressible	Viscous boundaries (Lysmer and Kuhlemeyer)	Yes	Y	Y
29	ANSYS	implicit	2.5 m	Acoustic-structural coupling	compressible	Viscous-spring artificial boundaries	No	Y	Y
30	ABAQUS	implicit	3.5 m	Acoustic-structural coupling	compressible	Infinite elements	Yes	Y	
31	ABAQUS	implicit	1.5 m	Acoustic-structural coupling	compressible	Viscoelastic artificial boundary	No	Y	Y
32	SOFISTiK	implicit	10 m	Fluid like structural elements	incompressible	Damper elements	No	Y	Y
33	ABAQUS	implicit	6 m	Acoustic-structural coupling	compressible	Infinite elements	No	Y	
34	ADINA	implicit	1 m	Fluid like structural elements	incompressible	Viscoelastic artificial boundary	Yes	Y	

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## Case D-1: Acceleration at point A. Comparison among peak values



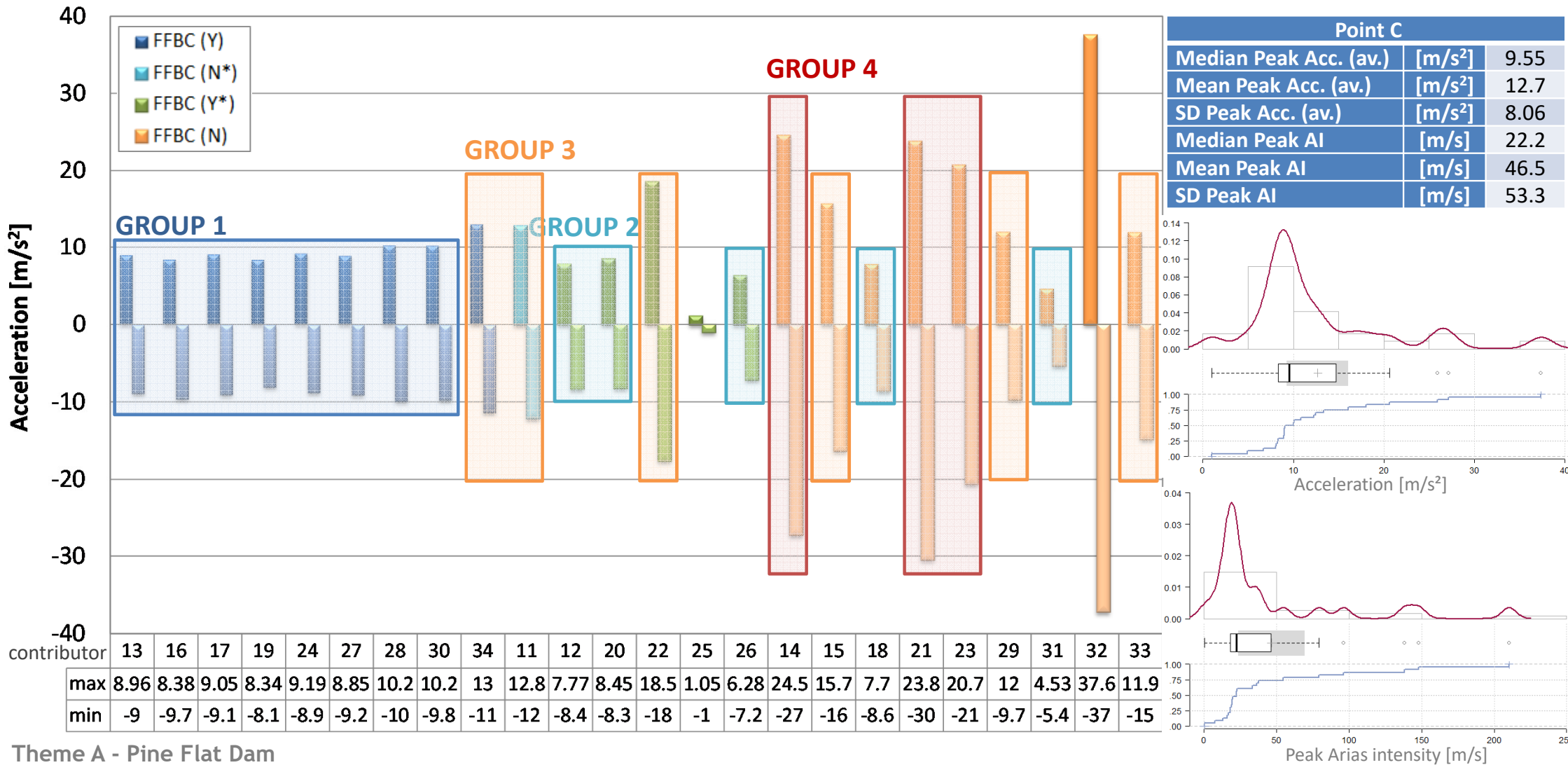
Point A		
Median Peak Acc. (av.)	[m/s <sup>2</sup> ]	1.46
Mean Peak Acc. (av.)	[m/s <sup>2</sup> ]	1.64
SD Peak Acc. (av.)	[m/s <sup>2</sup> ]	0.79
Median Peak AI	[m/s]	0.46
Mean Peak AI	[m/s]	0.56
SD Peak AI	[m/s]	0.31



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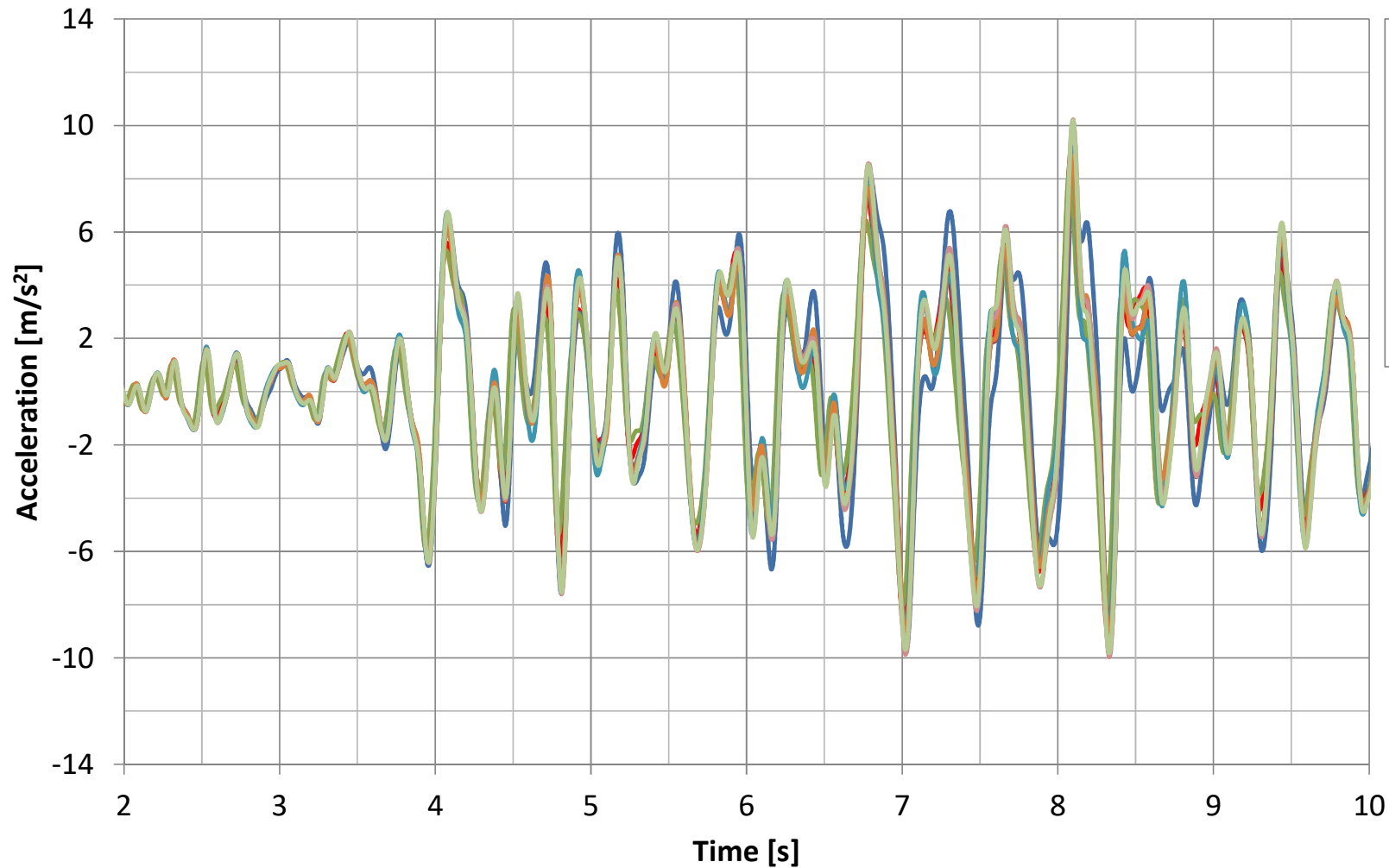


## Case D-1: Acceleration at point C. Comparison among peak values



Theme A - Pine Flat Dam

## Case D-1: Time history of Acceleration at point C (group 1)



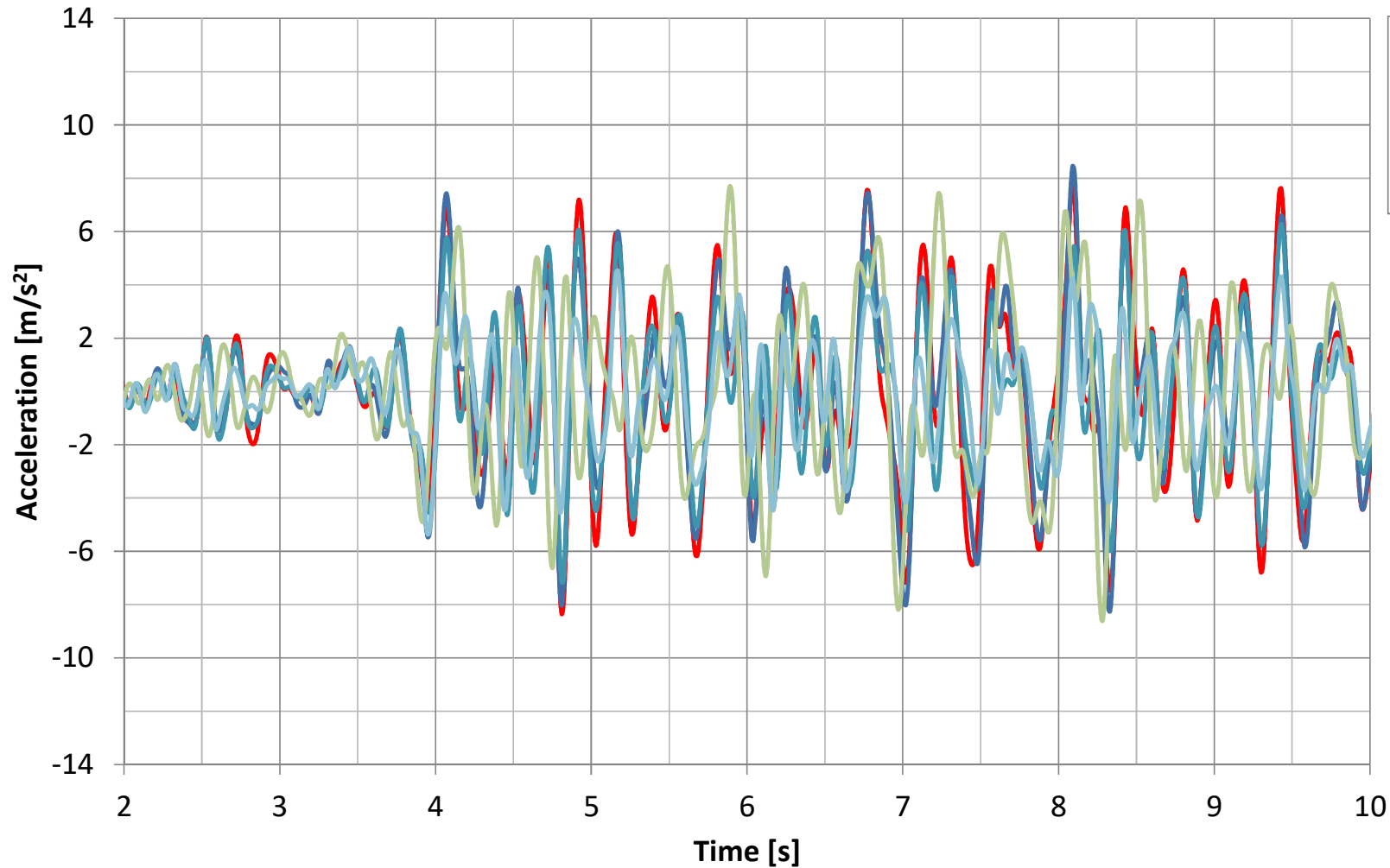
### GROUP 1

Contributors with FFBC & similar peak values

✓ Very good agreement also in the trend of acceleration.



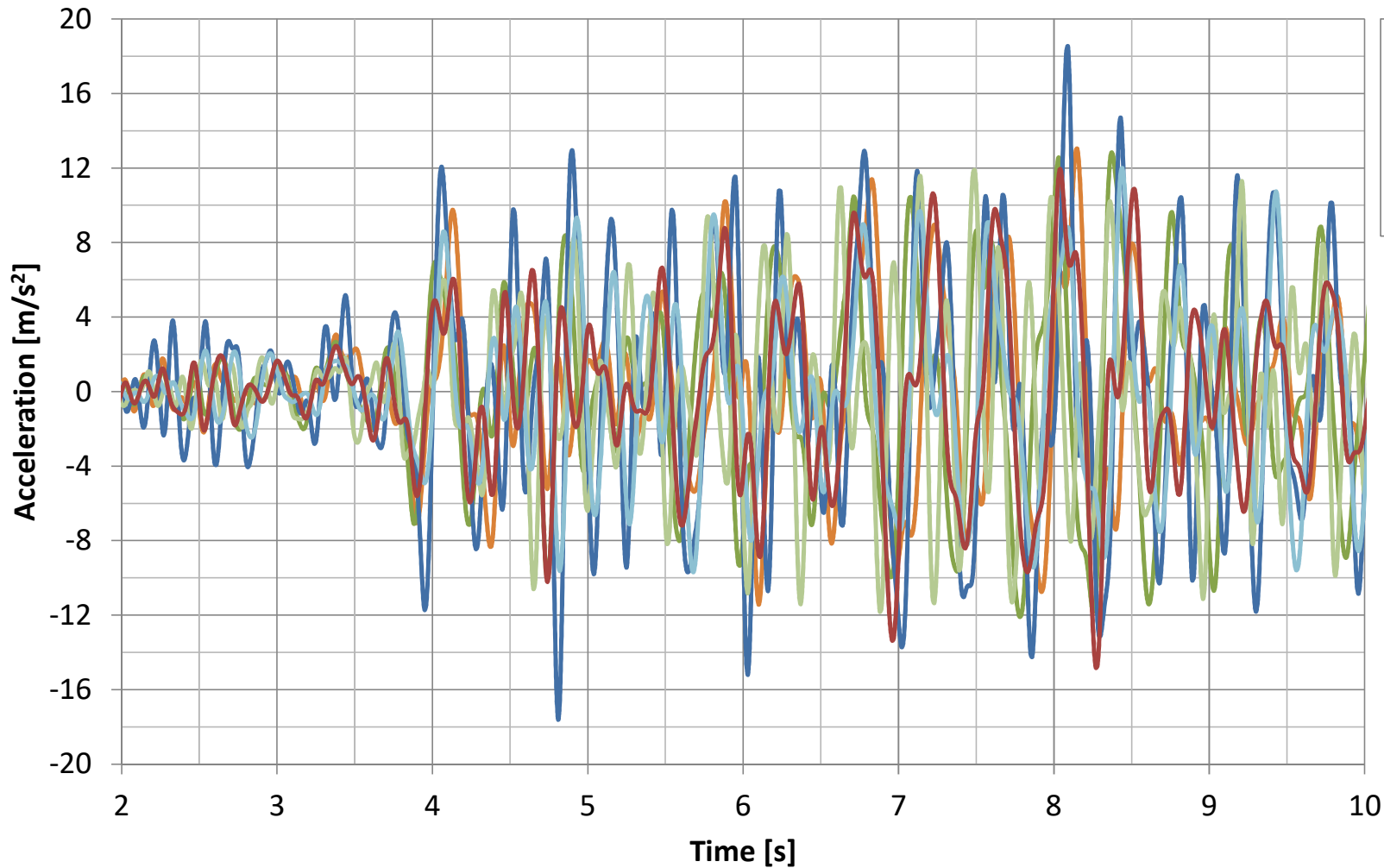
## Case D-1: Time history of Acceleration at point C (group 2)



**GROUP 2**  
Contributors without  
FFBC & with peak values  
lesser than  $10 \text{ m/s}^2$

✓ Fair agreement in the trend of acceleration: except for 18, peaks occur at the same time

## Case D-1: Time history of Acceleration at point C (group 3)

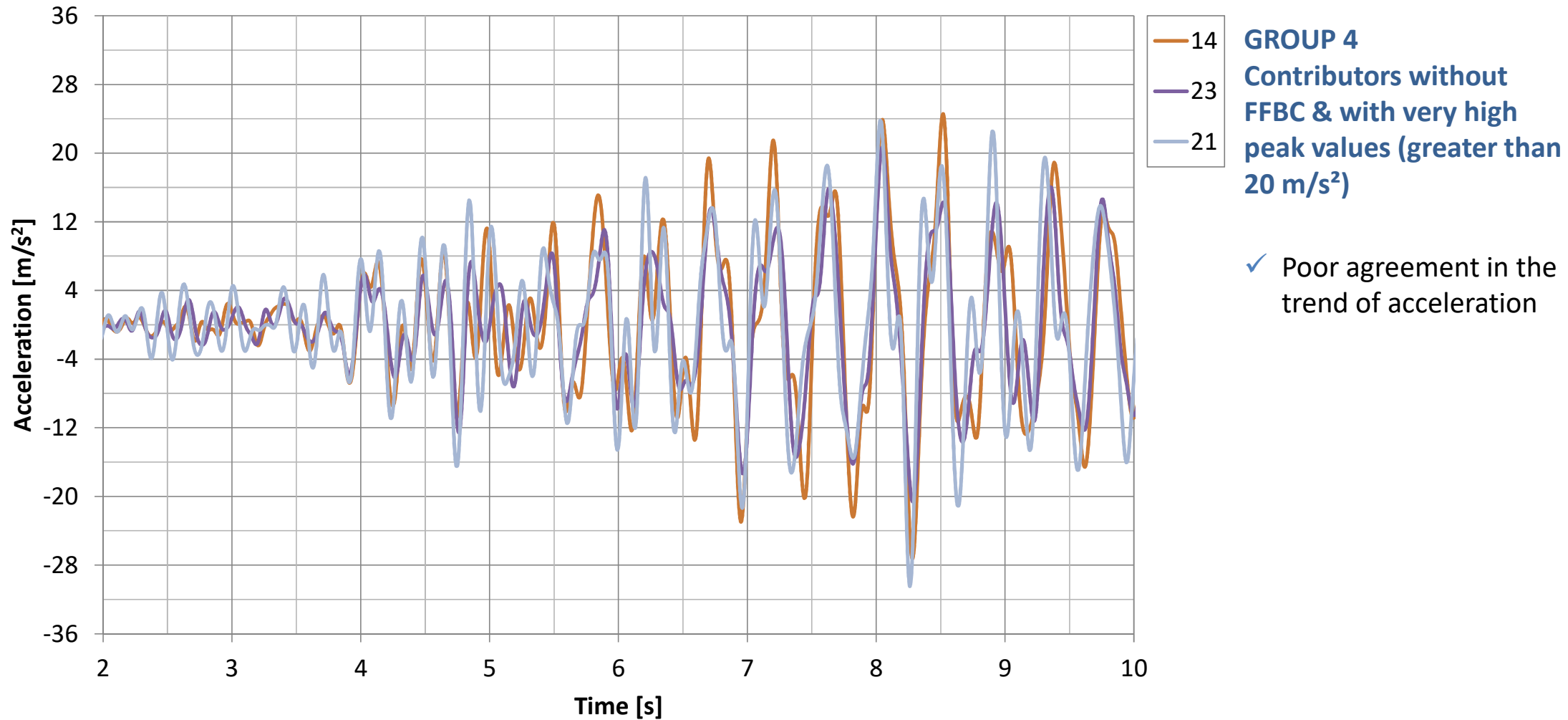


### GROUP 3

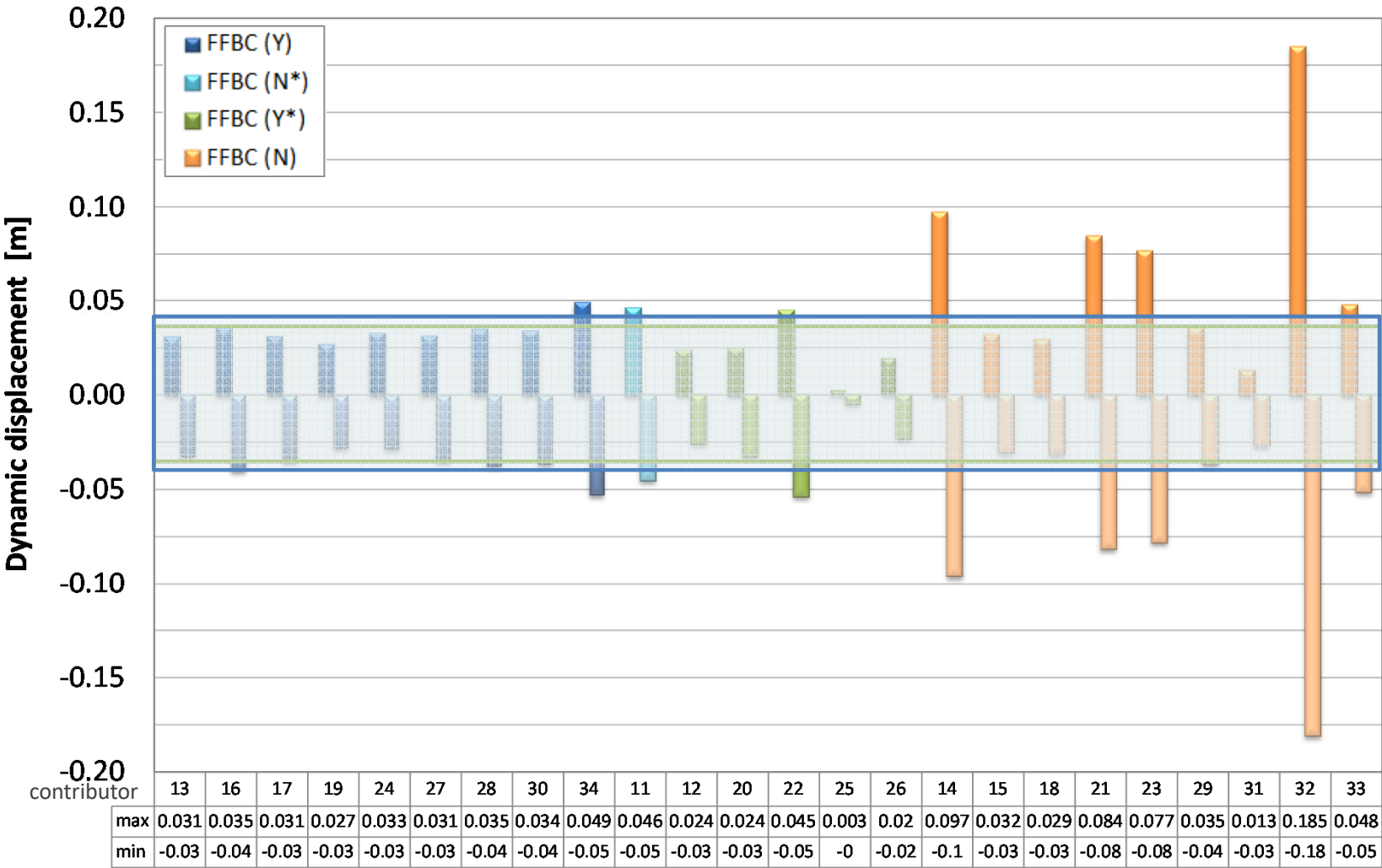
Contributors with and without FFBC & with peak values greater than 10 m/s<sup>2</sup>

✓ Poor agreement in the trend of acceleration

## Case D-1: Time history of Acceleration at point C (group 4)



Case D-1: Relative dynamic displacement at point C.  
Comparison among peak values

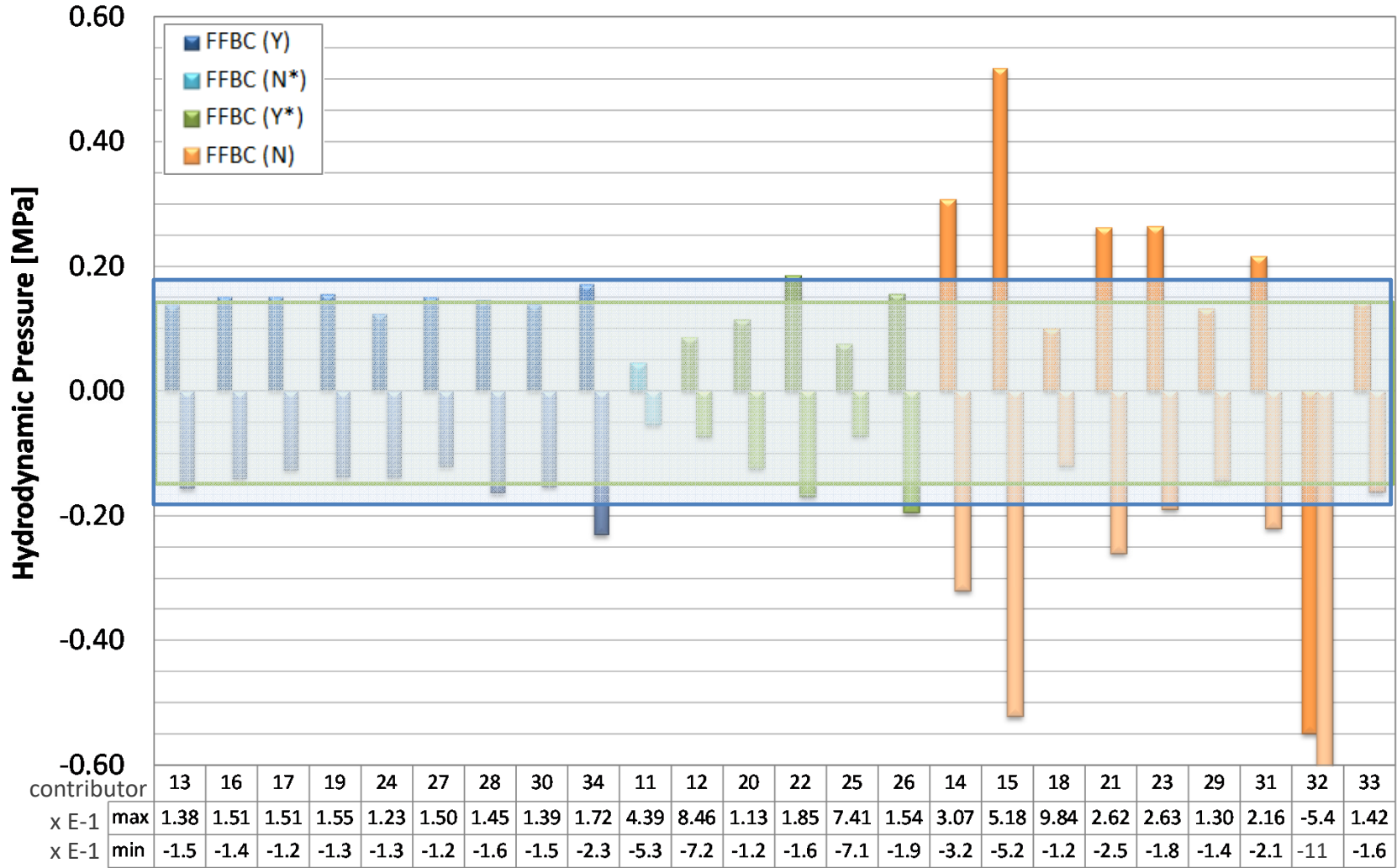


Point C		
Median Peak DD (av.)	[m]	3.29E-02
Mean Peak DD (av.)	[m]	3.93E-02
SD Peak DD (av.)	[m]	2.18E-02

Only Contributors with FFBC

Point C		
Median Peak DD (av.)	[m]	3.41E-02
Mean Peak DD (av.)	[m]	3.61E-02
SD Peak DD (av.)	[m]	7.13E-03

Case D-1: Hydrodynamic pressure at point A. Comparison among peak values

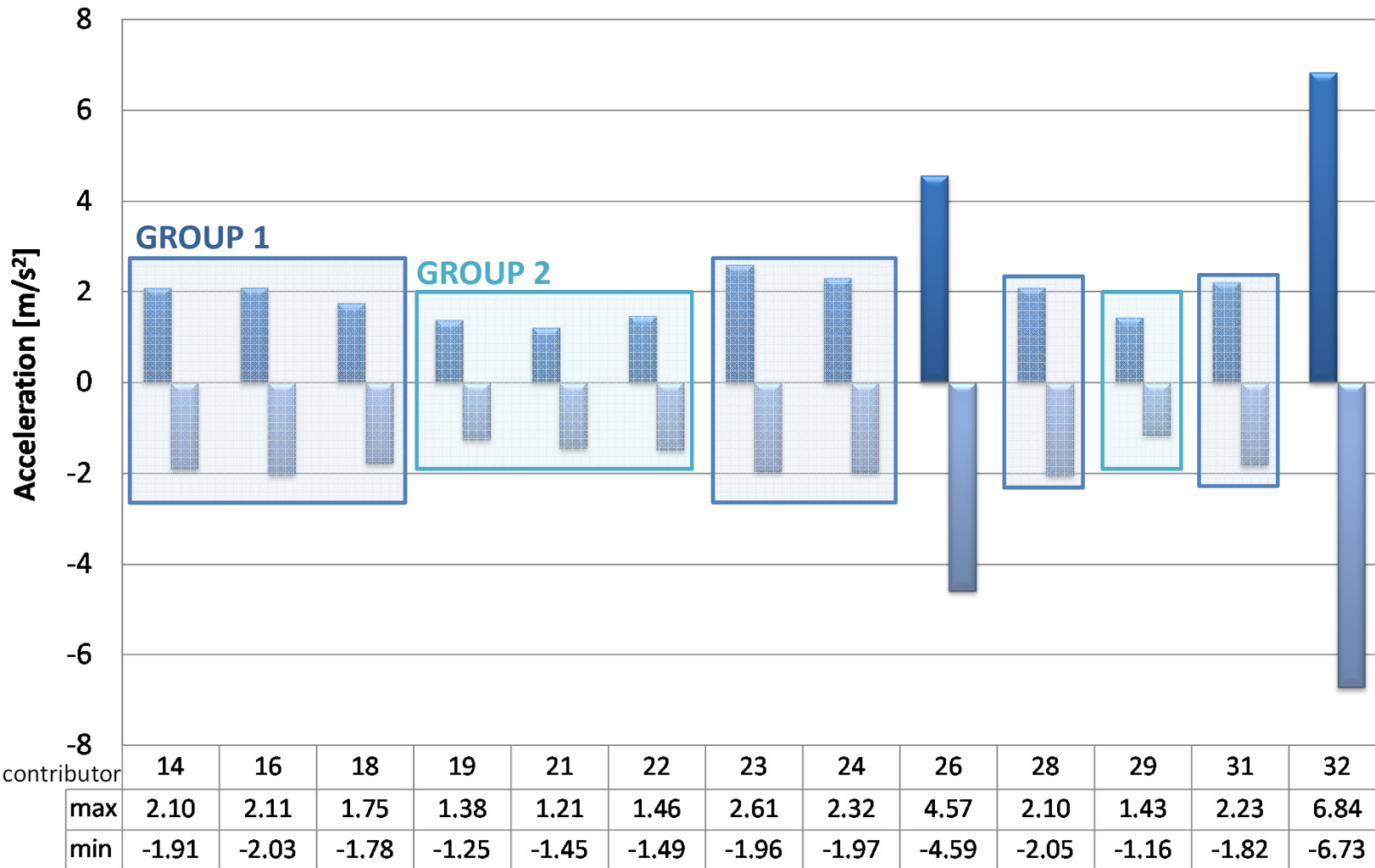


Point C		
Median Peak HP (av.)	[MPa]	0.147
Mean Peak HP (av.)	[MPa]	0.177
SD Peak HP (av.)	[MPa]	0.097

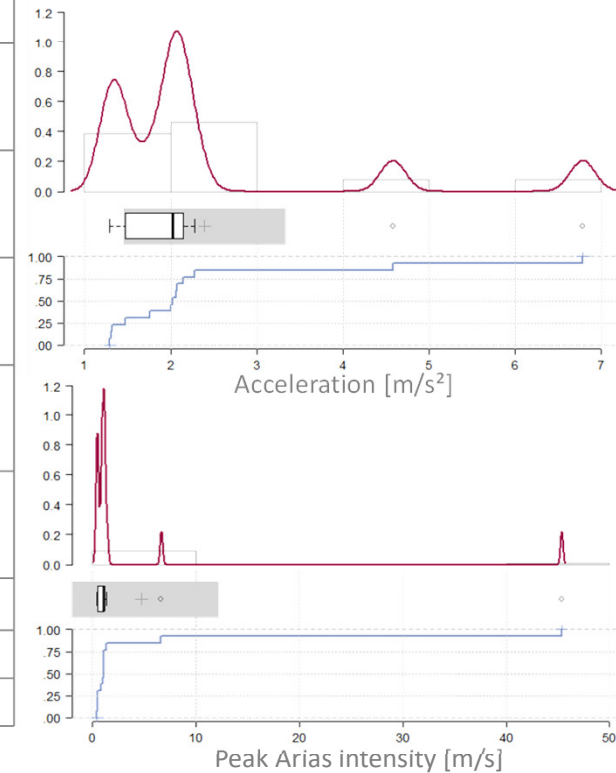
Only Contributors with FFBC

Point C		
Median Peak DD (av.)	[MPa]	0.146
Mean Peak DD (av.)	[MPa]	0.140
SD Peak DD (av.)	[MPa]	0.037

## Case F-1: Acceleration at point A. Comparison among peak values



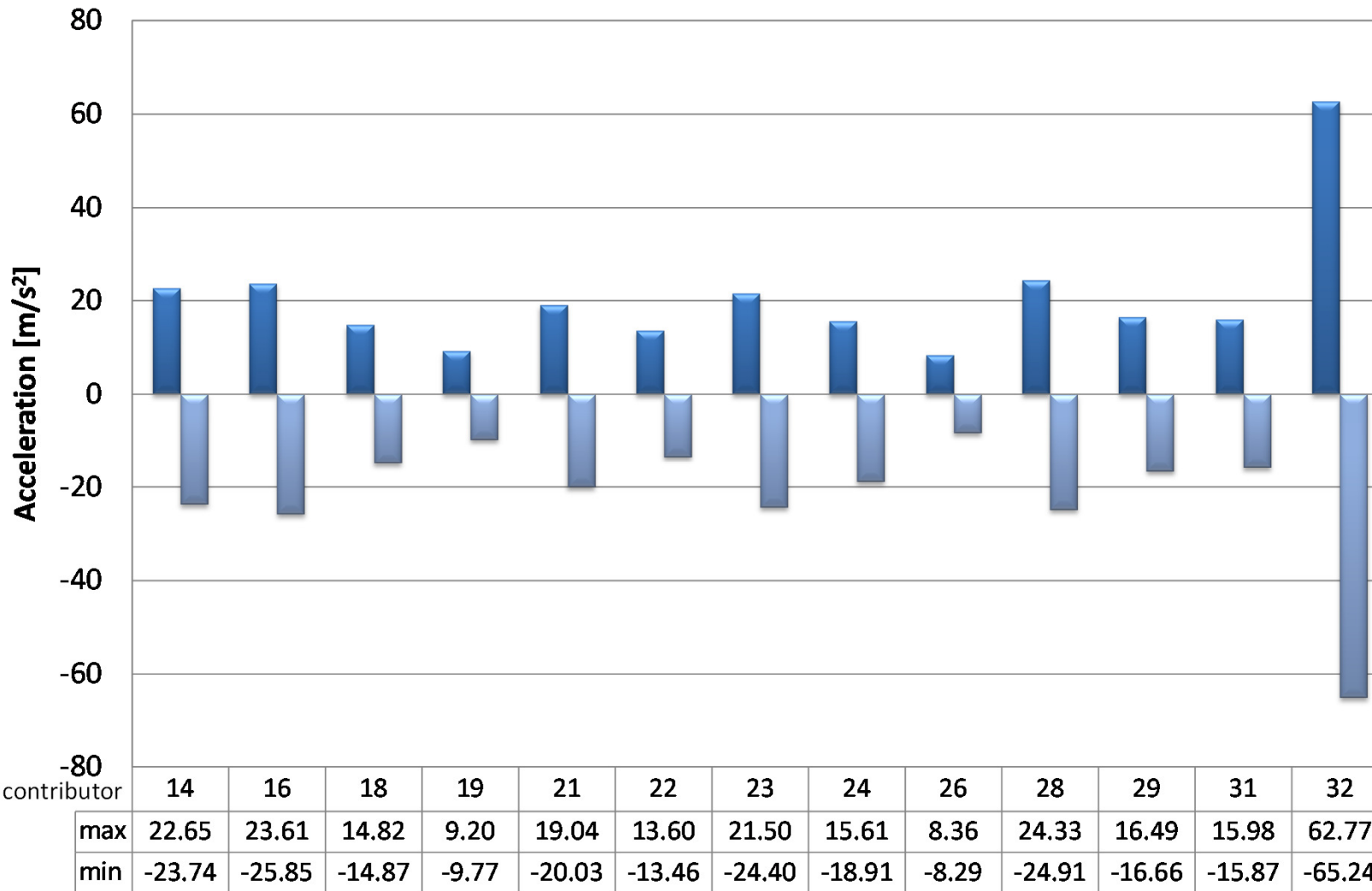
Point A		
Median Peak Acc. (av.)	[m/s <sup>2</sup> ]	2.03
Mean Peak Acc. (av.)	[m/s <sup>2</sup> ]	2.40
SD Peak Acc. (av.)	[m/s <sup>2</sup> ]	1.56
Median Peak AI	[m/s]	1.05
Mean Peak AI	[m/s]	4.71
SD Peak AI	[m/s]	12.3



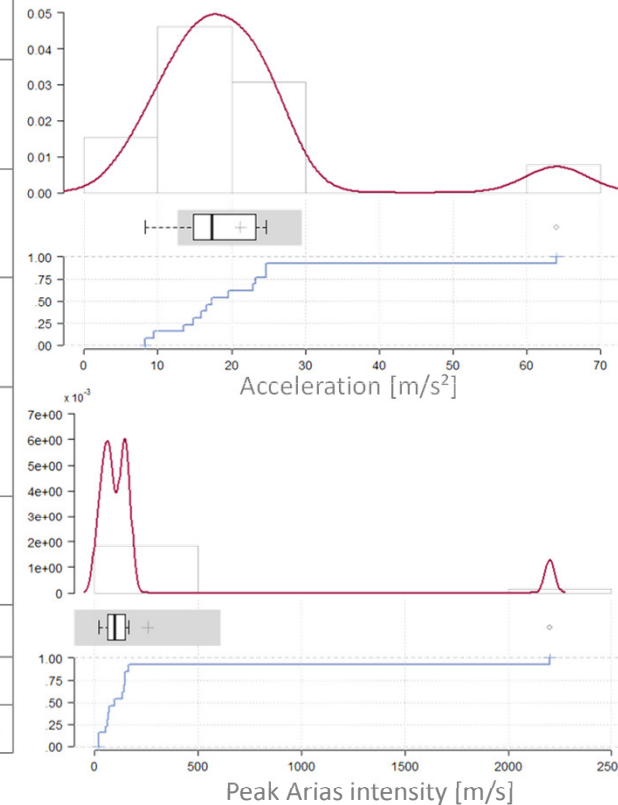
Theme A - Pine Flat Dam



## Case F-1: Acceleration at point C. Comparison among peak values



Point C		
Median Peak Acc.	[m/s <sup>2</sup> ]	17.3
Mean Peak Acc. (av.)	[m/s <sup>2</sup> ]	21.2
SD Peak Acc. (av.)	[m/s <sup>2</sup> ]	13.9
Median Peak AI	[m/s]	97.3
Mean Peak AI	[m/s]	256
SD Peak AI	[m/s]	587



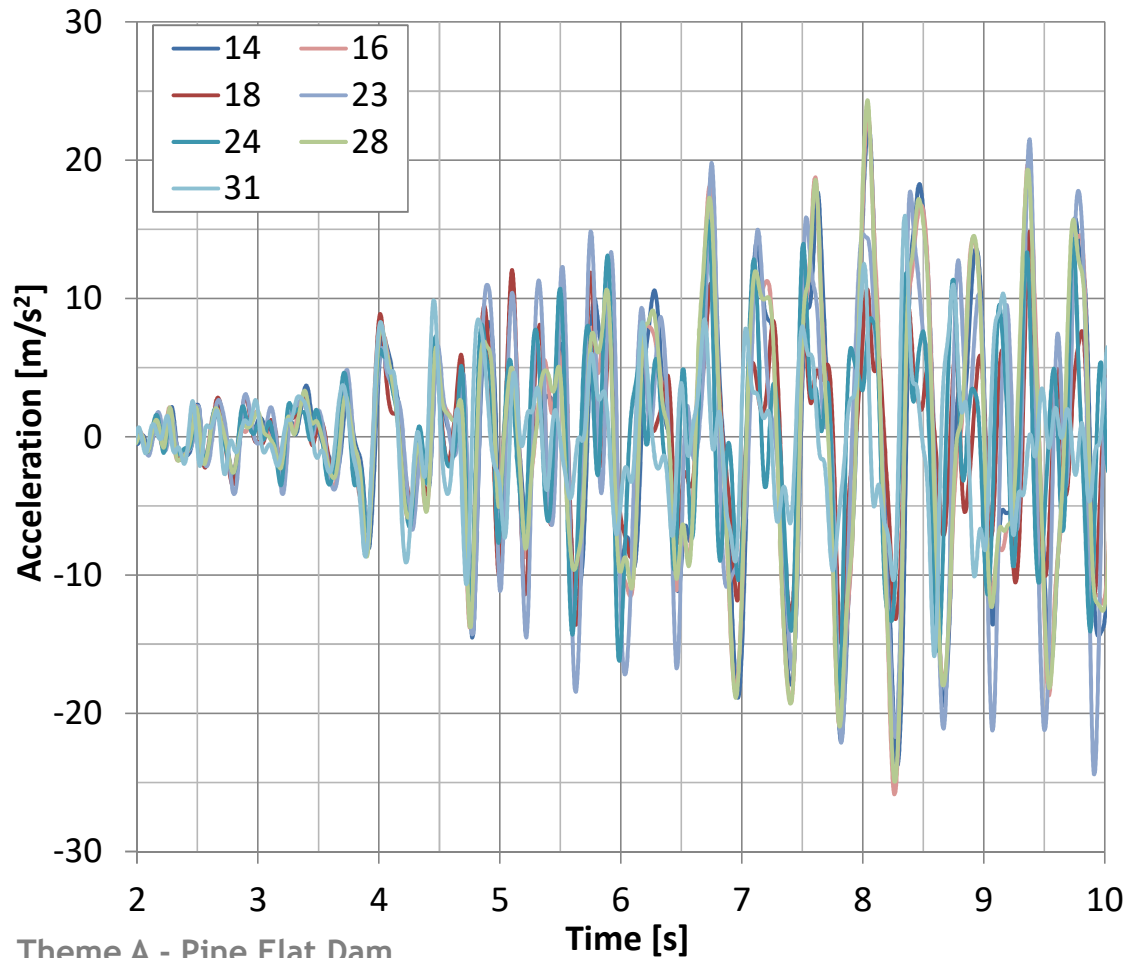
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## Case F-1: Time history of Acceleration at point C

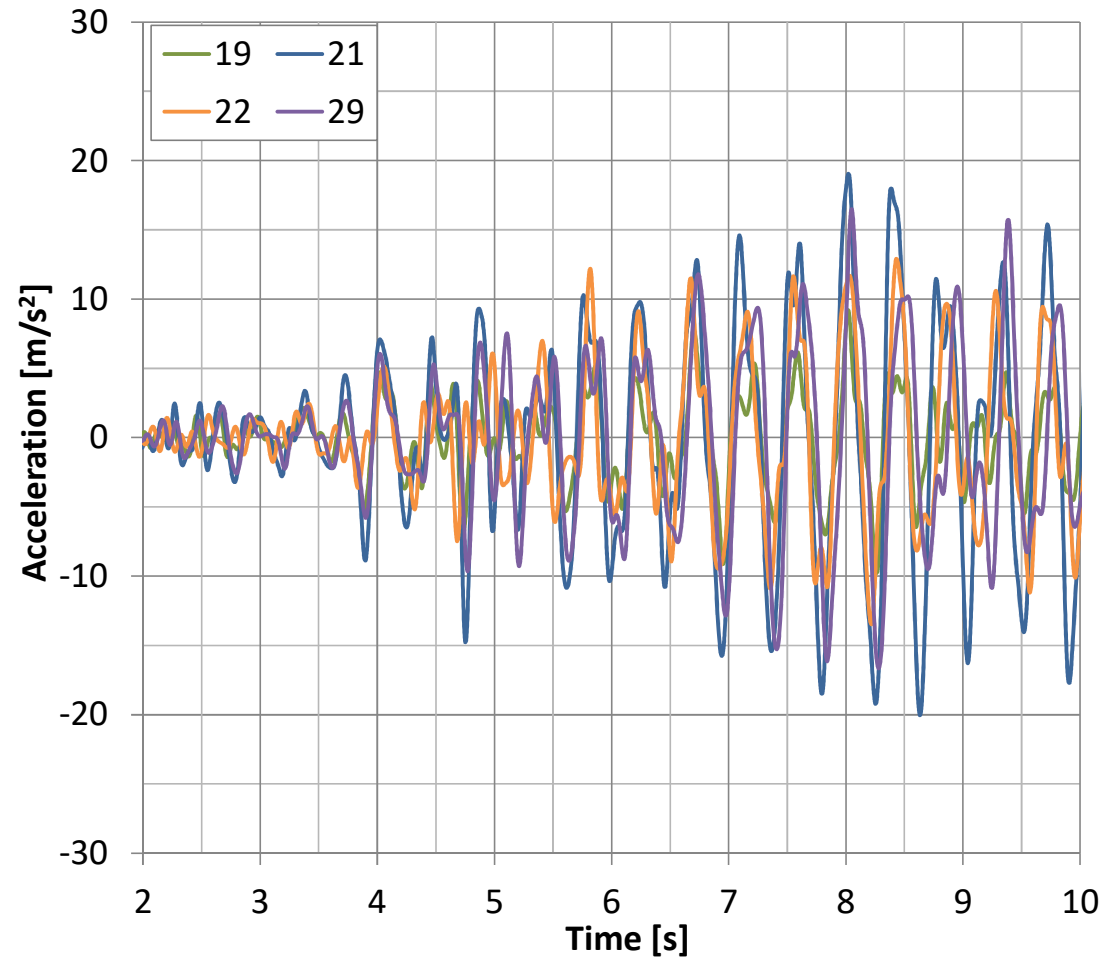
### GROUP 1

Peak Acceleration at Point A greater than  $1.77 \text{ m/s}^2$  (Taft PGA)



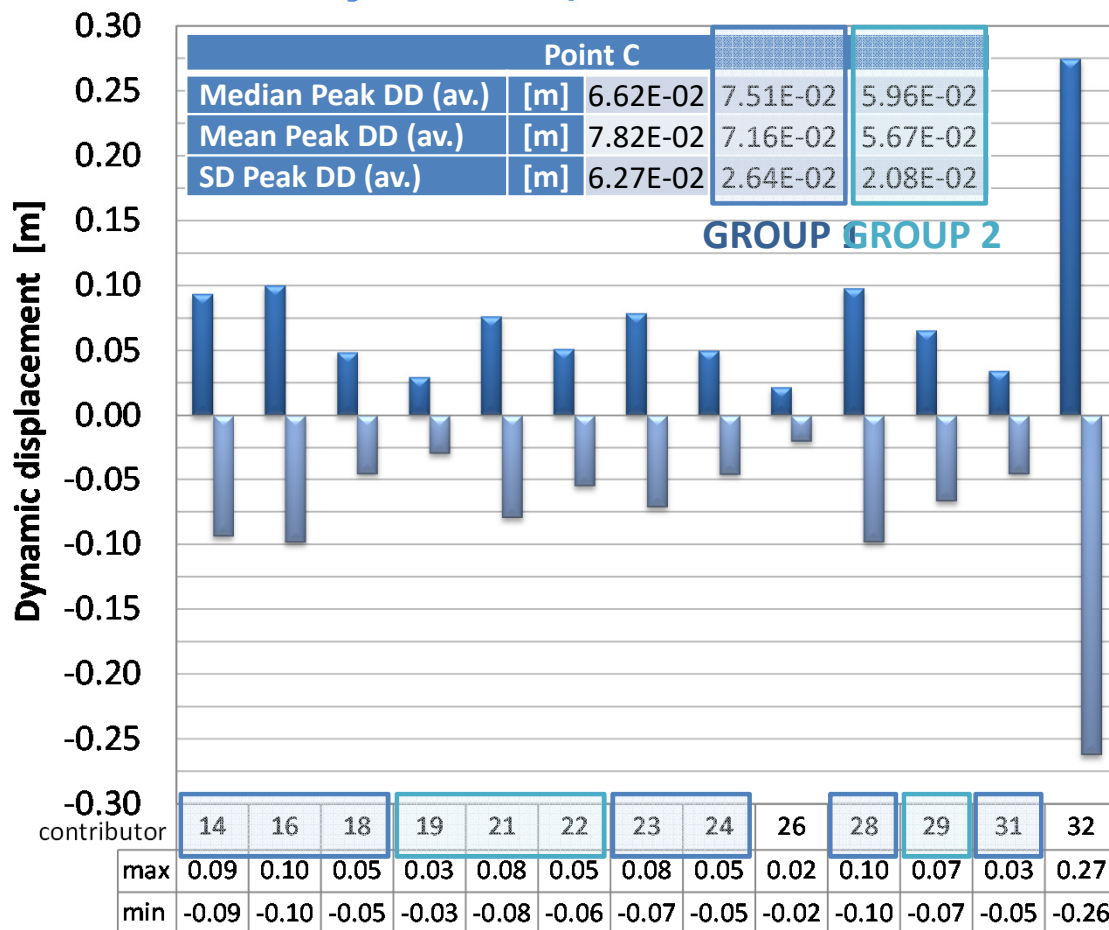
### GROUP 2

Peak Acceleration at Point A lesser than  $1.77 \text{ m/s}^2$  (Taft PGA)

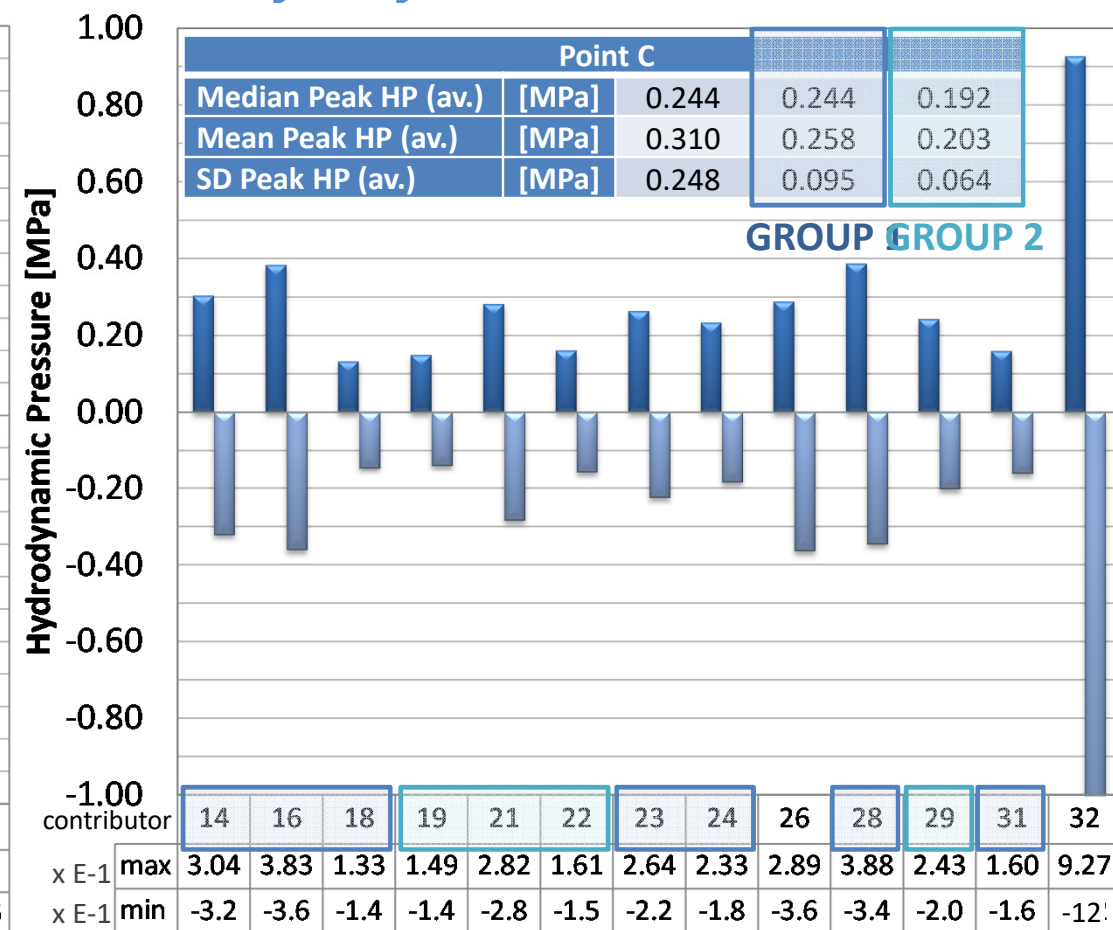


## Case F-1: Relative dynamic displacements and Hydrodynamic Pressure. Comparison among peak values

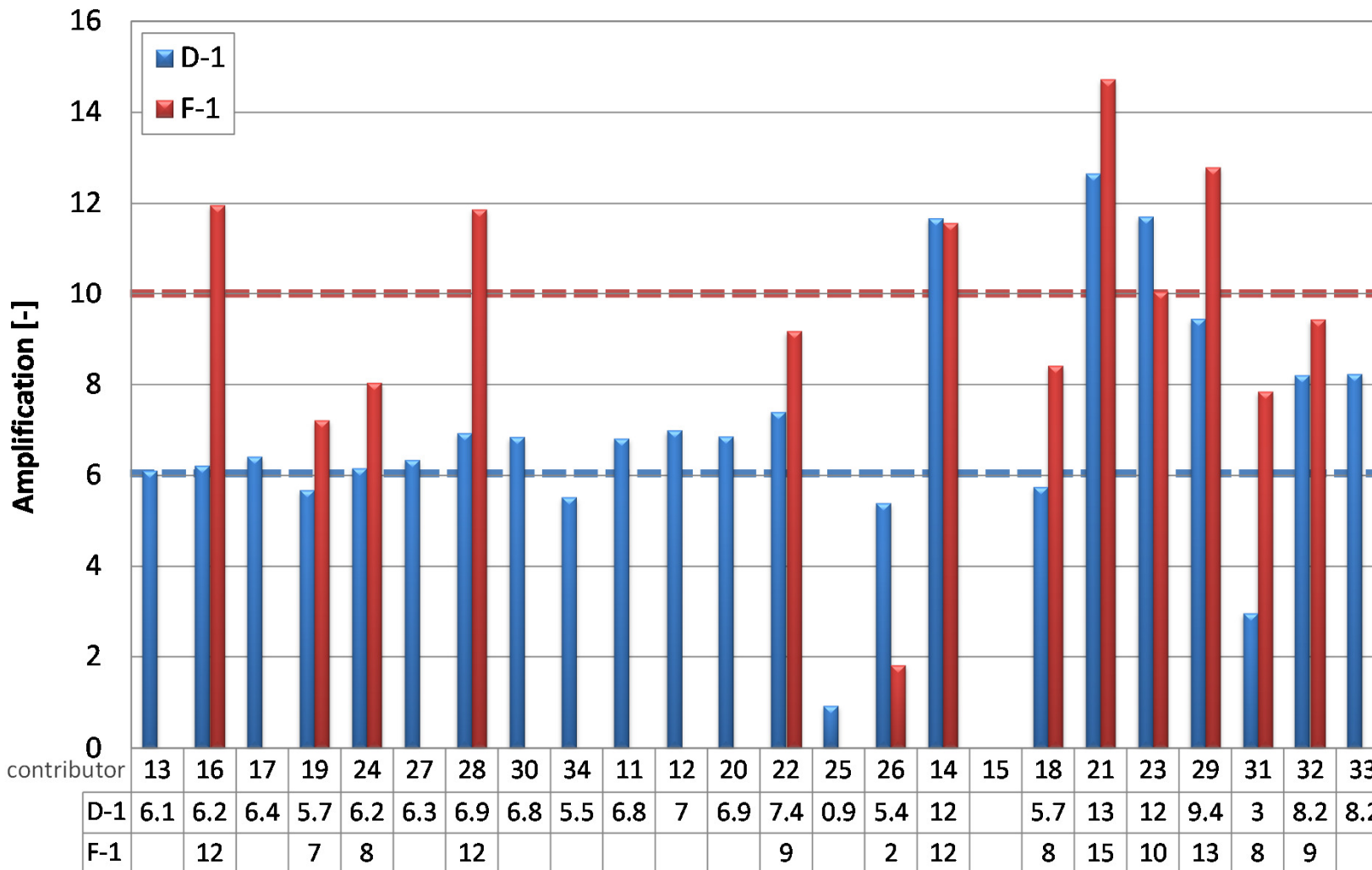
*Relative dynamic displacements at Point C*



*Hydrodynamic Pressure at Point A*



## Cases D-1 & F-1: Amplification of acceleration at point C



- Mean amplification in case D-1 (about 6) obtained considering only contributors with FFBC
- Mean amplification in case F-1 (about 10) obtained considering only contributors with Peak Acceleration at Point A greater than  $1.77 \text{ m/s}^2$  (Taft PGA)

**The models with the seismic wave propagation approach provide a less demanding seismic response of the system with respect to that achieved with the massless approach**

## Case D and Case F: final remarks



### ➤ **Models with seismic wave propagation approach**

A very good agreement is observed among contributors using the free-field boundary conditions. Results provided by contributors not using the free-field boundary conditions generally show higher variability to be further investigated.

### ➤ **Models with massless approach**

Results obtained from models with massless approach, although unexpectedly quite variable, confirm the general belief regarding the conservativeness of the method.